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► To cite this version:

Abderrahmane Bendali, M'Barek Fares, Sophie Laurens, Sébastien Tordeux. Numerical study of acoustic multiperforated plates. ESAIM: Proceedings, 2012, 37, pp.166-177. 10.1051/proc/201237005 . hal-00686434

HAL Id: hal-00686434

<https://hal.science/hal-00686434>

Submitted on 10 Apr 2012

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Numerical study of acoustic multiperforated plates

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April 6, 2012

Abstract

It is rather classical to model multiperforated plates by approximate impedance boundary conditions. In this article we would like to compare an instance of such boundary conditions obtained through a matched asymptotic expansions technique to direct numerical computations based on a boundary element formulation in the case of linear acoustic.

Introduction

Multiperforated boundaries are involved in several industrial devices (liners [11], mufflers [2], combustion chambers [12], noise barriers ...). The occurrence of a high density of holes of small size has a significant impact on the noise generated by the devices.

Until recently, it was almost impossible to predict the effect of a multiperforated plate by a direct numerical computation. To overcome this bottleneck, many authors have proposed to replace the perforated wall by an effective impedance boundary condition of transmission type, see [16] for the case of linear acoustic. This approach is suitable for numerical computation since it requires no mesh refinement in the neighborhood of the holes. The rapid increase of numerical computational abilities allows for the validation of this

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method by means of high performance computing. In this article, we would like to address such an issue using the parallel boundary element library CESC of CERFACS.

In section 1, we describe the considered geometry and state the boundary-value problem obtained by assuming that the equations of linearized acoustics are valid everywhere. In section 2, we briefly review some effective boundary conditions previously used for modeling multiperforated plates. Numerical experiments are presented in section 3.

1 Statement of the Problem

1.1 Description of the propagation domain

We consider an infinite waveguide \mathbb{T} with rectangular section

$$\mathbb{T} = \left\{ \mathbf{x} \in \mathbb{R}^3 : x_1 \in]0, h_1[\text{ and } x_2 \in]0, h_2[\right\}.$$

This domain is split into two parts by a multiperforated plate with zero thickness

$$\mathbb{P} = \left\{ \mathbf{x} \in \mathbb{R}^3 : x_1 \in]0, h_1[, x_2 \in]0, h_2[\text{ and } x_3 = 0 \right\}.$$

The wall \mathbb{P} is perforated by a grating of characteristic lengths η_1 and η_2 of holes Θ^m of radius $\delta > 0$

$$\left\{ \begin{array}{l} \mathbf{x}^m = \left(\frac{\eta_1}{2}, \frac{\eta_2}{2}, 0 \right) + ((m_1 + m_2\alpha)\eta_1, m_2\eta_2, 0) \text{ with } \alpha \in [0, 1[\\ \Theta^m = \{ \mathbf{x} \in \mathbb{R}^3 : \|\mathbf{x} - \mathbf{x}^m\| < \delta \text{ and } x_3 = 0 \} \\ \text{with } m \in \mathbb{S} = \left\{ (m_1, m_2) \in \mathbb{Z}^2 : \Theta^m \subset \mathbb{P} \right\}. \end{array} \right. \quad (1)$$

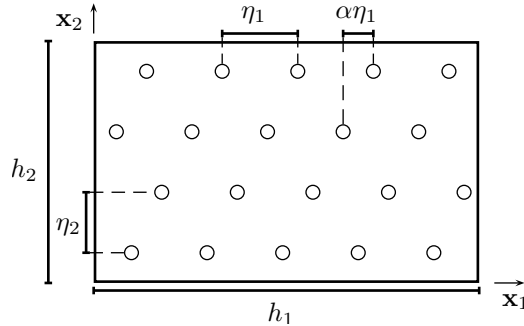


Figure 1: The multiperforated plate

The spacing between two holes is large enough so that short range interactions can be neglected, i.e., $\delta/\min(\eta_1, \eta_2) = o(1)$. We can thus define the propagation domain:

$$\Omega = \mathbb{T} \setminus \mathbb{P}_{\text{perf}} \text{ with } \mathbb{P}_{\text{perf}} = \mathbb{P} \setminus \left(\bigcup_{m \in \mathbb{S}} \Theta^m \right).$$

1.2 Linear acoustics modeling

The time variable and the speed of sound are respectively denoted by t and c . Let us recall that in the context of linear acoustic the pressure field $p : \Omega \times \mathbb{R}_+ \mapsto \mathbb{R}$ is governed by a scalar wave equation

$$\frac{\partial^2 p}{\partial t^2}(\mathbf{x}, t) - c^2 \Delta p(\mathbf{x}, t) = 0 \quad \text{in } \Omega.$$

The disturbed velocity vector field $\mathbf{v} : \Omega \times \mathbb{R}_+ \mapsto \mathbb{R}^3$ is linked to the pressure by linearized Euler's equations

$$\rho_0 \frac{\partial \mathbf{v}}{\partial t}(\mathbf{x}, t) + \nabla p(\mathbf{x}, t) = 0 \quad \text{in } \Omega,$$

where ρ_0 is the density of the fluid at rest. The boundary of the physical domain is supposed to be a perfectly rigid wall

$$\mathbf{v} \cdot \mathbf{n} = 0 \text{ on } \partial\Omega = \partial T \setminus \left(\mathbb{P} \setminus \left(\bigcup_{m \in \mathbb{S}} \Theta^m \right) \right),$$

with \mathbf{n} the normal unit vector outwardly directed to Ω . Considering a wave with pulsation ω and wave number $k = \omega/c$, we denote also by p and \mathbf{v} the phasors of respectively the pressure and the velocity

$$p(\mathbf{x}, t) = \Re \left(p(\mathbf{x}) \exp(-i\omega t) \right) \quad \text{and} \quad \mathbf{v}(\mathbf{x}, t) = \Re \left(\mathbf{v}(\mathbf{x}) \exp(-i\omega t) \right).$$

In the sequel we consider the well-posed boundary-value problem

$$\left\{ \begin{array}{l} \text{Find } p : \Omega \longrightarrow \mathbb{C} \text{ satisfying} \\ \chi p \in H^1(\Omega) \text{ for all } \chi \in \mathcal{D}(\mathbb{R}^3), \\ \Delta p(\mathbf{x}) + k^2 p(\mathbf{x}) = 0 \quad \text{in } \Omega, \\ \frac{\partial p}{\partial n}(\mathbf{x}) = 0 \quad \text{on } \partial\Omega, \\ p(\mathbf{x}) - \exp(ikx_3) \text{ is outgoing, see [4] or [10] for example,} \end{array} \right. \quad (2)$$

which provides a model for the time-harmonic waves standing in this acoustic system when it is fed by the propagating mode coming from $x_3 = -\infty$.

Remark 1. For a waveguide with small height and width ($kh_1 < \pi$ and $kh_2 < \pi$) the harmonic pressure p can be expressed as

$$\begin{cases} p(\mathbf{x}, t) = \exp(ikx_3) + R \exp(-ikx_3) + w_+(\mathbf{x}) & \text{for } x_3 < 0, \\ p(\mathbf{x}, t) = T \exp(ikx_3) + w_-(\mathbf{x}) & \text{for } x_3 > 0. \end{cases}$$

Parameters R and T are respectively the reflection and transmission coefficients. Both functions w_- and w_+ are evanescent in the x_3 direction (exponential decay):

$$w_-(\mathbf{x}) = o_{x_3 \rightarrow -\infty}(1) \quad \text{and} \quad w_+(\mathbf{x}) = o_{x_3 \rightarrow +\infty}(1).$$

2 The approximate transmission model for multi-perforated plates

For a large number of holes, even when resorting to high performance computing, the direct numerical solution of problem (2) is generally out of reach. To overcome this difficulty a solution consists in modeling the multiperforated plate by an equivalent transmission condition (also called impedance condition) which requires no mesh refinement.

These approximate conditions have been well-studied by the acoustic community both from the theoretical and experimental point of view. It can either be achieved using heuristic approaches based on a physical reasoning [16] or by means of asymptotic analysis, see [1], [2] or [3] and references therein. The last approach benefits from a rigorous framework based on the matching of asymptotic expansions techniques [9].

The conclusion of these studies can be physically interpreted as follows: the multiperforated plate can be modeled as an impenetrable moving membrane of surface mass ρ_S . This leads to a system of partial differential equations posed on the domain

$$\tilde{\Omega} = \mathbb{T} \setminus \mathbb{P}$$

governing the pressure field of the fluid \tilde{p} , the flow velocity vector field of

the fluid $\tilde{\mathbf{v}}$ and the surface velocity of the membrane $\tilde{\mathbf{V}} = (0, 0, \tilde{V}_3)$

$$\left\{ \begin{array}{l} \text{Acoustic equations in the fluid:} \\ \frac{\partial^2 \tilde{p}}{\partial t^2}(\mathbf{x}, t) - c^2 \Delta \tilde{p}(\mathbf{x}, t) = 0 \quad \text{in } \tilde{\Omega}, \\ \rho_0 \frac{\partial \tilde{\mathbf{v}}}{\partial t}(\mathbf{x}, t) + \nabla \tilde{p}(\mathbf{x}, t) = 0 \quad \text{in } \tilde{\Omega}, \\ \tilde{\mathbf{v}}(\mathbf{x}, t) \cdot \mathbf{n} = 0 \quad \text{on } \partial T. \\ \text{Impenetrability of the membrane:} \\ \tilde{v}_3(x_1, x_2, 0_-, t) = \tilde{v}_3(x_1, x_2, 0_+, t) = \tilde{v}_3(x_1, x_2, t). \\ \text{Second Newton's law for the membrane:} \\ \rho_S \frac{\partial \tilde{v}_1}{\partial t}(x_1, x_2, t) = \tilde{p}(x_1, x_2, 0_-, t) - \tilde{p}(x_1, x_2, 0_+, t). \end{array} \right.$$

In the case of an incident harmonic wave coming from $\mathbf{x}_3 = -\infty$, this system simplifies into a problem involving only $\tilde{p} : \tilde{\Omega} \rightarrow \mathbb{C}$

$$\left\{ \begin{array}{l} \chi \tilde{p} \in H^1(\tilde{\Omega}) \text{ for all } \chi \in \mathcal{D}(\mathbb{R}^3), \\ \Delta \tilde{p}(\mathbf{x}) + k^2 \tilde{p}(\mathbf{x}) = 0 \quad \text{in } \tilde{\Omega}, \\ \frac{\partial \tilde{p}}{\partial n}(\mathbf{x}) = 0 \quad \text{on } \partial T, \\ \frac{\partial \tilde{p}}{\partial x_3}(x_1, x_2, 0_- \text{ or } 0_+) = \frac{K_R}{A} \left(\tilde{p}(x_1, x_2, 0_+) - \tilde{p}(x_1, x_2, 0_-) \right), \\ \tilde{p}(\mathbf{x}) - \exp(ikx_3) \text{ is outgoing,} \end{array} \right. \quad (3)$$

expressed in terms of the so-called Rayleigh conductivity K_R of the hole and the surface of an unit-cell of the network $A = \eta_1 \eta_2$. These quantities are related to the surface mass of the membrane by:

$$\rho_S = \frac{\rho_0 A}{K_R}.$$

Remark 2 (Physical interpretation of the transmission condition). *In the theory of acoustics, it is well known that the effect of a small perforation in a rigid plate can be modeled by two acoustic point sources located on each side of the plate, see [16] for example. The algebraic fluxes of fluid coming from these sources Φ_- and Φ_+ are opposite (due to the conservation of mass) and related to the difference of pressure on the two sides of the plate $\tilde{p}_+ - \tilde{p}_-$ by an analogous relation to the second Newton's law:*

$$\rho_0 \frac{d\Phi_-}{dt} = -\rho_0 \frac{d\Phi_+}{dt} = K_R (\tilde{p}_+ - \tilde{p}_-).$$

The multiplicative constant K_R is traditionally called the Rayleigh conductivity, see [13]. It is given by

$$K_R = 2\delta$$

in the case of linear acoustics for a circular hole of radius δ in a plate of negligible thickness.

A fluid crossing a grating of holes has a complex structure in the neighborhood of the perforations but can be seen as a homogeneous fluid at large scale. The velocity of fluid is then determined by distributing over one unit cell of the network the flux coming from one hole :

$$\tilde{v}_3(x_1, x_2, 0_-, t) = -\frac{\Phi_-}{A} \quad \text{and} \quad \tilde{v}_3(x_1, x_2, 0_+, t) = \frac{\Phi_+}{A}.$$

This leads to the transmission conditions

$$\begin{cases} \tilde{v}_3(x_1, x_2, 0_-, t) = \tilde{v}_3(x_1, x_2, 0_+, t), \\ A \frac{\partial \tilde{v}_3}{\partial t}(x_1, x_2, 0_-, t) = \rho_0 K_R (\tilde{p}(x_1, x_2, 0_-, t) - \tilde{p}(x_1, x_2, 0_+, t)), \\ A \frac{\partial \tilde{v}_3}{\partial t}(x_1, x_2, 0_+, t) = \rho_0 K_R (\tilde{p}(x_1, x_2, 0_-, t) - \tilde{p}(x_1, x_2, 0_+, t)). \end{cases} \quad (4)$$

Remark 3. The solution of the approximate model can be analytically computed. Its solution depends only on the x_3 coordinate and is given by

$$\begin{cases} \tilde{p}_-(\mathbf{x}) = \exp(ikx_3) + \tilde{R} \exp(-ikx_3) & \text{for } x_3 < 0, \\ \tilde{p}_+(\mathbf{x}) = \tilde{T} \exp(ikx_3) & \text{for } x_3 > 0. \end{cases} \quad (5)$$

Inserting (5) in the transmission conditions (4) leads to the reflection and transmission coefficients:

$$\tilde{R} = \frac{-\frac{ikA}{K_R}}{2 - \frac{ikA}{K_R}} \quad \text{and} \quad \tilde{T} = \frac{2}{2 - \frac{ikA}{K_R}}.$$

3 A numerical experiment

We consider two multiperforated plates with almost the same geometrical characteristic lengths

$$h_1 = 5 \text{ cm}, \quad h_2 = 5 \text{ cm}, \quad \eta_1 = 5 \text{ mm}, \quad \eta_2 = 5 \text{ mm}, \quad \delta = 0.225 \text{ mm}.$$

In the first configuration, the grating is straight, $\alpha = 0$ (see (1) and Figure 1 for the definition of α) and tilted in the second one, $\alpha = 1/2$, see Figure 2.

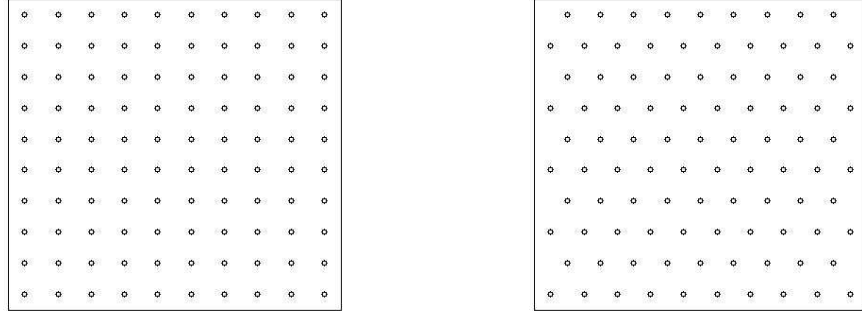


Figure 2: Multiperforated plates with $\alpha = 0$ and $\alpha = \frac{1}{2}$

The meshes, see Figures 3, were generated with the proprietary licensed software Altair HyperMesh library (<http://www.hyperworks.fr>) and its scripting language to ensure a local refinement in the neighborhood of each hole, see Figure 4.

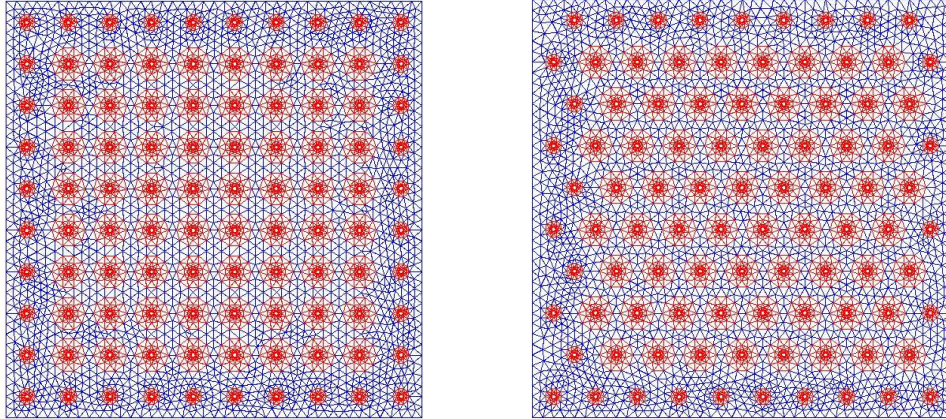


Figure 3: The meshes of the multiperforated plates for $\alpha = 0$ and $\alpha = 1/2$

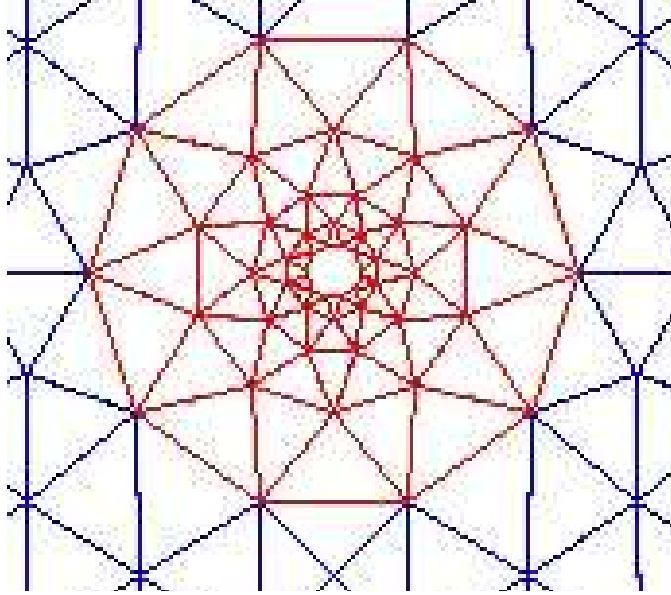


Figure 4: The local refinement Patch

The outgoing condition is approximated by truncating the domain at $h_3 = 2cm$ from the multiperforated plate, see Figure 5. On the two sections $x_3 = -h_3$ and $x_3 = h_3$ is prescribed the following accurate absorbing boundary conditions :

$$\begin{cases} \frac{\partial p}{\partial x_3}(x_1, x_2, -h_3) + ikp(x_1, x_2, -h_3) = 2ik \exp(ikh_3), \\ \frac{\partial p}{\partial x_3}(x_1, x_2, h_3) - ikp(x_1, x_2, h_3) = 0. \end{cases}$$

These conditions are rather accurate since they are obtained by neglecting the evanescent modes which are exponentially decaying.

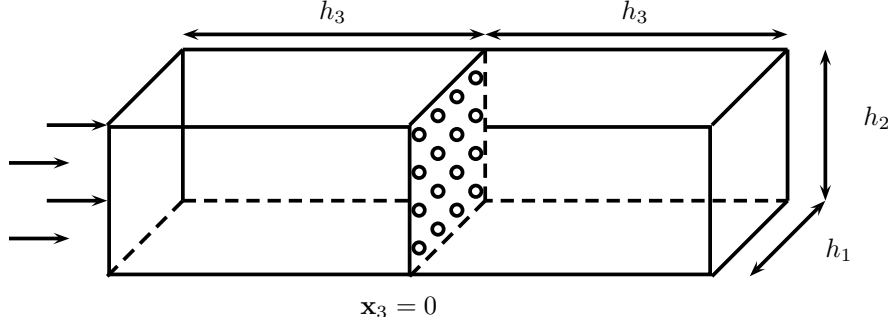


Figure 5: The truncated domain of computation

The numerical experiments have been achieved with the boundary element library CESC. We have chosen to use a double layer formulation [15] to discretize the system of equations (2) and numerically compute its reflection coefficient R . In order to check the convergence of the method, we have compared the numerical results with approximately 4×10^4 degrees of freedom (d.o.f.) to the results with 1.6×10^5 d.o.f. Both numerical approximations of the reflection coefficients coincide up to the third digit.

We have considered 26 frequencies (from 500 Hz to 3000 Hz with a 100 Hz step). The determination of the transmission and reflection coefficients at each frequency requires to form and invert a linear system with a dense matrix of approximately 40,000 unknowns. It was carried on a parallel platform having 400 processors. It required a rather large computational time ($5.2 \times 10^6 s$ i.e. $1.3 \times 10^4 s \cdot cpu^{-1}$).

The modulus $|R|$ and the phase angle of the reflection coefficients respectively obtained from the direct numerical solution and the homogenized approximate model are depicted in Figure 6 for the straight case ($\alpha = 0$) and in Figure 7 for the tilted case ($\alpha = 1/2$).

The conclusions that can be drawn from these plots are the following:

- As predicted by the theory, there is almost no difference between the straight case and the tilted case.
- Even if the overall behavior of the reflection coefficient is well predicted, an error of 10 % on its modulus and of 5 % on its phase angle can be observed.

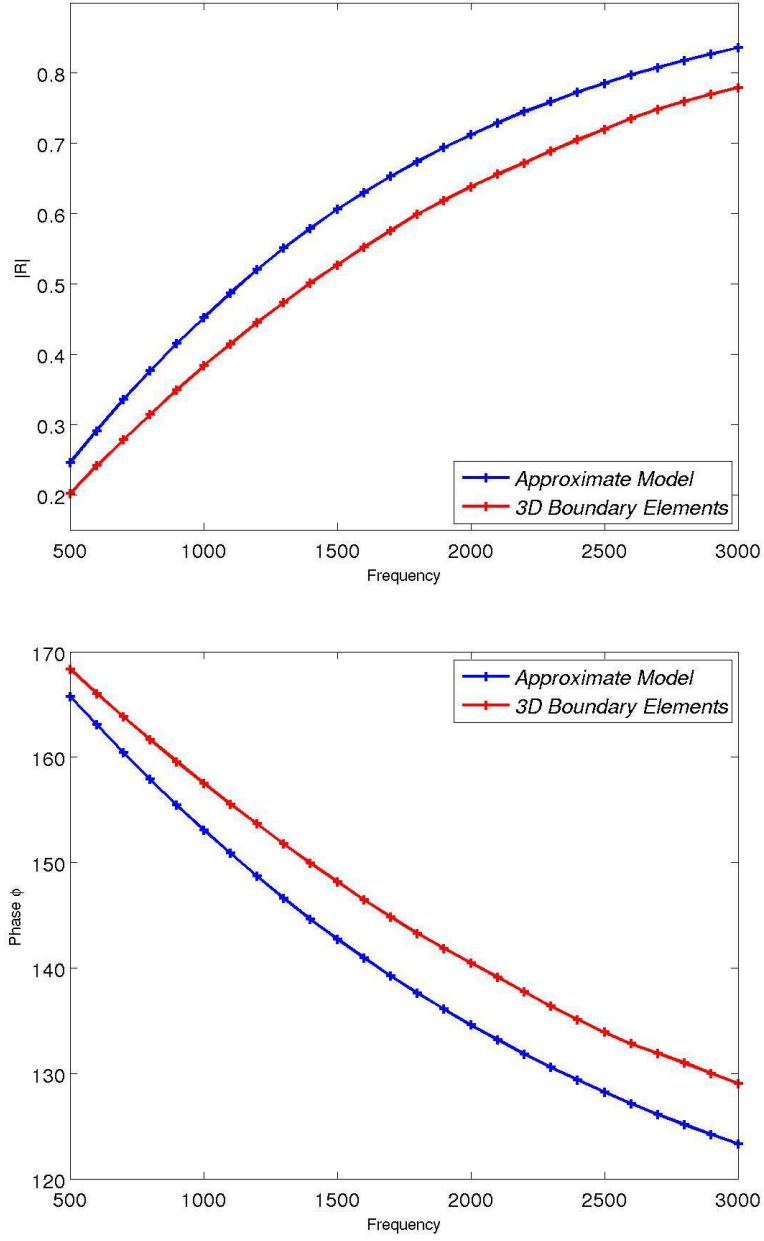


Figure 6: Comparison of the reflection coefficient $R = |R| \exp(i\phi)$ of the direct computations (green) and of the approximate model (blue) for straight multiperforated plate

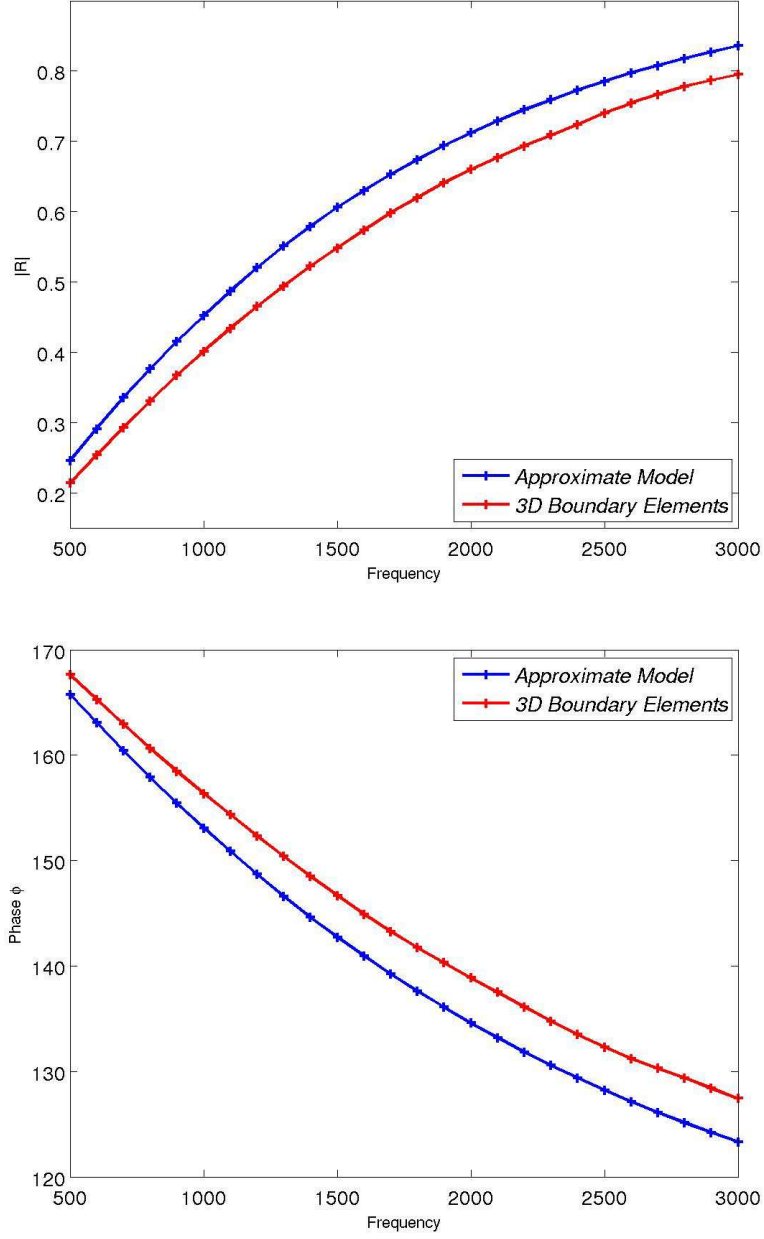


Figure 7: Comparison of the reflection coefficient $R = |R| \exp(i\phi)$ of the direct computations (green) and of the approximate model (blue) for the tilted multiperforated plate

4 Conclusion

A numerical validation of the approximate transmission condition modeling the reflection and the transmission of acoustic waves by a multiperforated plate has been carried out. The modulus and the phase angle for the reflection coefficients obtained through a direct numerical solution and the use of the homogenized transmission condition have exactly the same overall behavior even if a discrepancy between the two results gives rise to an error of about 10 %. To reduce this discrepancy, it would be interesting in our opinion to carry out further investigations.

First, the homogenized transmission conditions can be improved by taking into account the short range interactions. These objectives can be achieved by performing a multi-scale in place of a two-scale asymptotic analysis.

Moreover, in most applications (combustion chamber, liners), linear acoustics is not generally used for modeling the behavior of the acoustic field in the proximity of the holes. Reproducing this approach for these more complicated models seem to be rather challenging. One can refer to [14] for viscosity and to [6, 7, 8] for aeroacoustic effect.

The last issue is the choice of the numerical method. We have chosen to use a direct solution by a plain boundary element method without accelerating it by a Fast Multipole Method (FMM) (see, e.g., [5]). This choice is motivated by the fact that the problem being considered here is in the low frequencies range and at the best of authors knowledge no completely satisfactory FMM is available in this case.

Acknowledgments.

This work was supported by the French National Research Agency under grant no. ANR-08-SYSC-001.

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